EMSA OP/10/2013

A STUDY ASSESSING THE ACCEPTABLE AND PRACTICABLE RISK LEVEL OF PASSENGER SHIPS RELATED TO DAMAGE STABILITY

08 September 2015
Content

- Introduction and overview of the EMSA III studies (Odd Olufsen)
- Formal Safety Assessment, Risk Models for collision and grounding (Rainer Hamann)
- Methodologies for assessing risk from watertight doors and risk from grounding (Odd Olufsen)
- Sample ships; design and risk control options (Henning Luhmann)
- Summary of results, recommendations for decision making (Odd Olufsen)
Members of the consortium

- **Shipyards:**
  - EUROYARDS, representing: Meyer Werft, Fincantieri, Meyer Turku, STX-France
- **Designers/Consultants:**
  - Knud E. Hansen AS & Safety at Sea
- **Operators:**
  - Carnival Cruise, Color Line, Royal Caribbean & Stena Line
- **Universities:**
  - National Technical University of Athens, University of Strathclyde & University of Trieste
- **Software developer:**
  - Napa OY
- **Classification Society:**
  - DNV GL
Background

- Passenger ships transport significant numbers of persons compared to cargo ships.
- Therefore, safety of persons on board is in focus in passenger ship design.
- The main risk contributors for passenger ships are accidents leading to loss of watertightness, i.e. collision, contact and grounding.
- Currently designed ships need to comply with SOLAS 2009 probabilistic damage stability requirements.
- SOLAS 2009, to a great extent, was based on research work of the HARDER project.
- When introducing SOLAS 2009, the level of R was based on the safety level of the current fleet.
## Overview of completed tasks in the EMSA III project

<table>
<thead>
<tr>
<th>Task</th>
</tr>
</thead>
<tbody>
<tr>
<td>Risk acceptance criteria and risk based damage stability</td>
</tr>
<tr>
<td>Evaluation of risk from watertight doors</td>
</tr>
<tr>
<td>Evaluation of risk from grounding</td>
</tr>
<tr>
<td>Damage stability calculations of GOALDS design</td>
</tr>
<tr>
<td>Combined assessments</td>
</tr>
</tbody>
</table>
Defined tasks and their main elements

Task 1: **Acceptable and practicable risk level of passenger ships**
- Risk level in comparison with other transport modes
- Updated collision risk model
- Risk control options (RCo) and cost benefit assessment (CBA)
- Recommending level of the required index R

Task 2: **Evaluation of risk from watertight doors**
- Collecting records; onboard monitoring cruise and RoPax
- Parametric model reflecting number, categorisation and closing time of WTD
- Parametric model developed and used to assess risk on the sample ships
- RCo and CBA carried out for some sample ships

Task 3: **Evaluation of risk from grounding**
- Updated damage statistics and grounding risk model including contact damages
- Side and bottom grounding damage statistics
- NAPA software developed for direct generation of hull breaches from statistics
- Attained index for grounding damages
- Calculations of A carried out on all sample ships
- RCo and CBA carried out for some sample ships

Task 4: Combined assessment of cost effectiveness of previous parts, FSA compilation and overall recommendation for decision making.
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FSA and risk models

- In 2002 IMO agreed that adjustment/development of regulations should be prepared using risk analysis (→ Formal Safety Assessment Guidelines)

- Goals of this study:

  could damage stability requirements of passenger ships be increased following FSA process

- This study considers

  - Passenger ships: cruise, passenger, RoPax and RoPax-Rail

  - Ships in compliance with current damage stability requirements (reference)
FSA

- FSA was developed to support IMO decision making by helping to evaluate regulatory changes in terms of benefits and related costs.
- FSA should provide recommendations for decision making.

FSA
- Comprises a complete risk assessment
  - Hazard identification
  - Risk assessment
  - Risk reduction measures
  - Cost-benefit assessment
  - Reporting
- Suggests required safety level to be tolerable and ALARP.
Tolerable and ALARP

- Tolerable and ALARP means
  - That risk is not intolerable (→ risk reduction without cost-benefit assessment)
  - ALARP process is applied

- ALARP process:
  - Measures reducing risk (frequency, consequence or both) are identified/developed
  - Measures are assessed with respect to benefits (safety, economic) and costs by
    - Risk reduction is quantified
    - Costs of risk reduction measures are determined
    - Measures are assessed in terms of cost/risk reduction ratio and a criterion specified in FSA Guidelines

ALARP = As Low As Reasonable Practical
ALARP process

- FSA guidelines provide criteria for cost benefit assessment
  - Gross cost of averting a fatality ($GCAF$) $GCAF = \frac{\Delta \text{Cost}}{\Delta \text{Risk}}$
  - Net cost of averting a fatality ($NCAF$) $NCAF = \frac{\Delta \text{Cost} - \Delta \text{Benefit}}{\Delta \text{Risk}}$
  - An RCO is cost beneficial if $GCAF/NCAF$ are equal to or lower than threshold

- Threshold for $GCAF$ and $NCAF$ provided by FSA Guidelines ($3$ million)
- Threshold were determined by means of specified process using social indicators (not static, follows general development)
- The value given in FSA Guidelines was suggested in 1999 (MSC 72/16) considering social indicators until 1988
- In GOALDS project threshold was updated to $7.45$ million
- In this study $4$ and $8$ million has been used.
EMSA III study

1. Definition of Goals, Systems, Operations
2. Hazard Identification
3. Scenario Definition
4. Cause and Frequency Analysis
5. Consequence Analysis
6. Options to decrease Frequencies
7. Options to mitigate Consequences
8. Cost-Benefit Assessment
9. Risk Controlled?
10. Reporting

Risk models
Cost-Benefit Analysis
Recommendation
Development of risk model

- Analysis of casualty reports to determine main events characterising risk
  - Develop high-level event sequence
- Analysis of accident statistics to specify representative sample
  - Development of annual accident frequencies
- Select/review casualty reports
- Develop risk model, e.g. in form of event tree
- Quantify risk model
  - Initial accident frequency
  - Dependent probabilities
    - Numerical model
    - Historical data
    - Expert judgement
Definition of sample

- **Basis:**
  - IHS Fairplay casualty database and ship register
  - Lloyds Maritime Investigation Unit database (LMIU)
  - Global Integrated Ship Information System (GISIS)

- **Sample characteristics of ships**
  - Built after 1981
  - ≥ 1000 gross tonnage
  - ≥ 80 m
  - IACS class at time of accident/today
  - No High Speed Crafts
Casualties cruise

CN (serious and not serious collision) accidents between 1994 and 2012 distinguishing IACS and Non IACS cruise ships.
Casualties RoPax

The graph shows the frequency of casualties in RoPax (Roll-on Roll-off Passenger and Cargo) ships from 1994 to 2012. The x-axis represents the years, and the y-axis represents the frequency of casualties.

- **RoPax CN** (blue bars)
- **RoPax CT** (purple bars)
- **RoPax GR** (orange bars)

The data indicates a significant increase in casualties in 2008, with a peak frequency of approximately 0.005. Thereafter, the frequency decreases in subsequent years.
Casualty database

- Basis for this study formed the casualty database developed in GOALDS project extended by reports after 2009
- All records were reviewed and populated accordingly
- By review process casualty reports not relevant for this study were identified and not further considered
- Initial casualty information is coming from IHS database. This information was enhanced from other sources especially in cases where accident investigating reports were available (e.g. GISIS)
- Only casualties considered complying with filtering criteria (ship size, year built etc.)
Risk Model

- For the purpose of this study two risk models were developed for accident categories
  - Collision
  - Grounding (+ contact)
- Only consequences with respect to persons on board are in focus
- Quantitative risk model developed using Event Tree method
- Ship type dependent risk models were developed separately for cruise and RoPax, in order to considering particularities, e.g. for
  - Initial accident frequencies
  - Fatality rates
- Risk models are ship size dependent, with respect to
  - Number of person on board
  - Probability of sinking
Risk Model: Collision

- High-level event sequence for collision casualties of passenger ship
  - Considers main factors influencing the risk to persons on board
Risk Model: Quantification

- Initial accident frequency

<table>
<thead>
<tr>
<th>Time Period</th>
<th>Cruise</th>
<th>RoPax</th>
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<tbody>
<tr>
<td>1994 - 2012</td>
<td>19, 5.78E-03, 17, 6.36E-03</td>
<td>52, 7.72E-03, 50, 9.38E-03</td>
</tr>
</tbody>
</table>

- Initiator: Struck/striking
  - Small number of casualty reports providing sufficient information for quantifying nodes of risk model
  - Therefore, in the view of reducing uncertainty, casualty reports for cruise and RoPax were merged
  - On average struck/striking probability is about 50% (struck: 43% cruise, 58% RoPax)
  - Analysis of casualty reports showed that collision accident damages are only relevant for ship stability when ship is struck
Risk Model: Quantification

- Operational area
  - Extent of hull damage heavily relates to impact energy which depends on ship speed and mass
  - In terminal area extent of hull damage is smaller than for collision in open sea or coastal waters
  - In order to adequately consider this two operational areas were distinguished
    - Terminal with typical low speed operation and ships berthed
    - All other areas
  - Quantification was based on casualty reports merging cruise and RoPax ships (33 reports)
Risk Model: Quantification

- Water ingress
  - Depends on
    - Whether hull is penetrated in collision
    - Location of the breach, i.e. is water ingress possible

- By distinguishing two operational areas the model considers the differences between operation in terminal areas and others:
  - Probability of water ingress in terminal areas is about 7% (based on 14 casualty reports)
  - Probability of water ingress in other areas is about one third (based on six reports)
  - Quantification was based on casualty reports merging cruise and RoPax ships
Risk Model: Quantification

- Probability of sinking
  - Is determined on basis of SOLAS 2009 damage stability requirements
  - Probability of sinking equal to 1 minus attained index (A-Index)

- Consequences
  - Related to persons on board (crew + passengers)
  - Considering occupancy of 90% for cruise, respectively seasonal occupancy for RoPax (100% for 12.5% of the year, 75% for 25% of the year and 50% for remaining time)
  - Two representative fatality rates used for the scenarios
    - Fast sinking/capsizing 80% of persons on board
    - Slow sinking 5% of persons on board
    - For sinking in terminal areas 5% fatality rate used for all scenarios
    - Probability of fast sinking depends on ship type (18% for cruise, 50% for RoPax)
Collision risk model

Initial acc. Freq.: ship category dependent

Collison risk model

Prob. Fast sinking: Ship type dependent (18% cruise, 50% RoPax)

Based on merged casualty reports (cruise, RoPax)

Fatality rates: same for cruise and RoPax, depend on sinking velocity

Prob. Sinking: SOLAS 2009 1-A -> ship type and ship size (PoB) dependent

Ungraded
- High-level event sequence for grounding and contact casualties of passenger ship
- Contact casualties with potential of penetrating hull and subsequent water ingress
- Only consequences with respect to persons on board are in focus
Risk Model: Quantification

- Initial accident frequency

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<tr>
<th>Time Period</th>
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<th>RoPax</th>
</tr>
</thead>
<tbody>
<tr>
<td>2000 - 2012</td>
<td>20 + 22 1.57E-02</td>
<td>27 + 86 2.12E-02</td>
</tr>
</tbody>
</table>

- No of casualties 1/ship year

- Cruise: 20 + 22, 1.57E-02
- RoPax: 27 + 86, 2.12E-02
Risk Model: Quantification

- Operational state
  - Considering that scenarios will differ between accidents in terminal areas and other areas, e.g. with respect to possibility of rescue but also water depth
  - About 57% of accidents occurred in terminal areas (217 reports for period 1990 to 2012)
- Damage location
  - Distinguishing between side and bottom damage
  - For terminal areas about 92% are side damages (75 casualty reports)
  - For other areas about 51% are bottom damages (43 casualty reports)
Risk Model: Quantification

- Nodes *staying aground* and *hull breach*
  - Consider influences like sea bed (soft/hard) or the general probability of hull breach (side damage)
  - Additionally, the possibility of staying aground was considered (= no possibility of sinking)
Risk Model: Quantification

- **Probability of sinking**
  - Is determined on basis of the new developed model
  - Similar to collision the probability of survival is expressed in terms of an index ($A_{GR}$-Index)

- **Consequences**
  - Related to persons on board (crew + passengers)
  - Considering occupancy of 90% for cruise, respectively seasonal occupancy for RoPax (100% for 12.5% of the year, 75% for 25% of the year and 50% for remaining time)
  - Two representative fatality rates used for the scenarios
    - Fast sinking/capsizing 80% of persons on board
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Cost-benefit assessment

- Risk models are used to determine risk reduction by increased damage stability
- Risk models are based on experience and numerical models
- For cost-benefit assessment so-called cost thresholds were calculated by means of risk models, i.e. calculating risk reduction (difference between A-Indices of reference and novel design) and monetary value per avoided fatality
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The effect of open watertight doors

\[ r(t=5\text{min}) = 1 - c(t) \times \frac{Vcn}{VDH} \]

\[ c(t) = 1.047 \times (1 - \exp(-0.104 \times t)) \]
A parametric model that can be used for assessing risk from watertight doors has been developed:

\[
\begin{align*}
    r^* &= \frac{A_{\text{opened}}^*}{A_{\text{closed}}^*} = 1 - b \frac{V_{\text{cn all}}}{V_{DH}} \\
    b &= \frac{\sum_{i=1}^{n_{\text{door}}} P_{\text{WTD}_i} \cdot c(t_i) \cdot V_{\text{cn}_i}}{\sum_{i=1}^{n_{\text{door}}} V_{\text{cn}_i}}
\end{align*}
\]
## Categorisation of watertight doors

<table>
<thead>
<tr>
<th>Door Category</th>
<th>Description of category</th>
<th>Probability that a door is open at a certain point of time $P_{WTD_i}$</th>
<th>Time to close the door, $t_i$</th>
</tr>
</thead>
<tbody>
<tr>
<td>A</td>
<td>Door permitted to stay open at sea</td>
<td>100%</td>
<td>5 minutes</td>
</tr>
<tr>
<td>B</td>
<td>Door which may be opened during work in the vicinity of the door</td>
<td>60%</td>
<td>3 minutes</td>
</tr>
<tr>
<td>C</td>
<td>Door which may be used to pass through</td>
<td>11%</td>
<td>1 minute</td>
</tr>
<tr>
<td>D</td>
<td>Door which is always closed – this is proposal of a new door category</td>
<td>0%</td>
<td>0 minute</td>
</tr>
</tbody>
</table>
Methodology for assessing survivability from grounding

- Probabilistic method for grounding.pptx
Sample ships, Risk Control Options and Cost Benefit Assessment

- Introduction and overview of the EMSA III studies (Odd Olufsen)
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EMSA3 Sample ships and design teams
Overview EMSA III  Sample ships

<table>
<thead>
<tr>
<th>Yard/Designer</th>
<th>Type</th>
<th>Length bp (m)</th>
<th>B (m)</th>
<th>T (m)</th>
<th>GT</th>
<th>Number of persons</th>
</tr>
</thead>
<tbody>
<tr>
<td>MW</td>
<td>Large cruise</td>
<td>294.6</td>
<td>40.8</td>
<td>8.75</td>
<td>153400</td>
<td>6730</td>
</tr>
<tr>
<td>Fincantieri</td>
<td>Small cruise</td>
<td>113.7</td>
<td>20.0</td>
<td>5.30</td>
<td>11800</td>
<td>478</td>
</tr>
<tr>
<td>Meyer Turku</td>
<td>Baltic RoPax</td>
<td>232.0</td>
<td>29.0</td>
<td>7.20</td>
<td>60000</td>
<td>3280</td>
</tr>
<tr>
<td>STX-France</td>
<td>Med RoPax</td>
<td>172.4</td>
<td>31.0</td>
<td>6.60</td>
<td>43000</td>
<td>1700</td>
</tr>
<tr>
<td>KEH</td>
<td>Small RoPax</td>
<td>95.5</td>
<td>20.2</td>
<td>4.90</td>
<td>7900</td>
<td>625</td>
</tr>
<tr>
<td>KEH</td>
<td>Double ender</td>
<td>96.8</td>
<td>17.6</td>
<td>4.30</td>
<td>6245</td>
<td>610</td>
</tr>
</tbody>
</table>

- Sample ships are suitable examples for state-of-the-art designs
- Basic design level
  - feasible realistic design to meet business model
  - No detailed layout of structure, architectural layout, piping and ducting
Overview EMSA III Sample ships

**Number of persons vs Length**

- Cruise
- Ropax
- GOALDS Cruise
- Sample ships cruise
- GOALDS Ropax
- Sample ships Ropax

**Attained index A for sample ships**

- SOLAS2009 75% in lifeboats
- SOLAS2009 30% in lifeboats
- GOALDS sample ships
- EMSA3 Sample Ships

Attained index for Ropax based on SOLAS2009, impact of S-wod (SLF55) not shown.
Design variations

- For each sample ship design variations (RCOs) have been developed
- Following modifications have been applied in different combinations
  - Change of breadth and freeboard
  - Improvement of watertight subdivision
  - Different hull form
  - Buoyancy boxes on the car deck
  - Subdivided LLH
- For each RCO the change of A and costs have been calculated
Calculation assumptions

- SOLAS2009 is used as calculation base
  - Assumptions as in Explanatory Notes
  - For RoPax additional new S-wod according SLF55 calculated
  - Draught range based on loading conditions
  - A-class boundaries considered in flooding stages
- Assumptions:
  - The business model is kept constant
    - No significant change of capacity (cargo, cabins)
    - Operational profile kept the same (distance, turn around time)
  - Same methodology to calculate weight and stability
  - Simplified but realistic cost estimations
  - GM limit curve defined based on loading conditions
  - Margins to GM curve are kept constant
- No detailed internal watertight integrity considered
  - Projects are on basic design level
  - No detailed routing of pipes and ducts
Cost-Benefit Assessment

- Cost Benefit Assessments for sample ships are based on:
  - **Investment Costs**
    - Building costs due to enlarged ship (steel, interior systems)
    - Cost impact due to changed equipment (engines, propulsion, thrusters etc)
    - Financing costs
  - **Operational costs**
    - Mainly fuel costs
    - Increased time in port may cause increased speed → higher fuel costs
    - Increased maintenance costs
  - **Revenue**
    - Small adjustments of income
    - Reduced probability of total loss results in less costs for scrap

- All costs are calculated in Euro and converted in USD based on exchange rate of 1.35 USD/Euro
- Changes of costs to the society or industry in general due to changed probability of large accidents have not been accounted for
Fuel oil price development

- Data published by EIA energy outlook have been used as basis for estimating the future trends.

- The current prices for HFO and MGO; 600 USD/t and 900 USD/t, have been obtained using the average reported prices for 2013 and 2014 in Rotterdam using Clarkson Intelligence as a source.

- The price of LSHFO is obtained based on a 20/80 distribution of the HFO and MGO price. This is the distribution that is required in order to obtain a content of 0.5 % sulphur.

- Price of LNG is taken as 94.1% of the MGO cost. This is a standard assumption used in analysis based on the LNG supplier’s standard way of pricing where it is referred to that the cost of the LNG should correspond to 80% of the use of MGO.

- The latest reduction of fuel prices (MGO 540 USD/t, HFO 300 USD/t) has not been accounted for.
Cost Effectiveness

- For each ship the relation between ΔA and Δcosts created using the netCAF limits of 4Mio USD and 8Mio USD.
- This allows a simple check, if an RCO meets the criteria for cost effectiveness
Large cruise vessel – Meyer Werft & Carnival

<table>
<thead>
<tr>
<th>Length bp (m)</th>
<th>B (m)</th>
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Ungraded
Large cruise vessel – Meyer Werft & Carnival

- Global changes (beam, freeboard)
- Local changes (internal subdivision)

<table>
<thead>
<tr>
<th>Version</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>G2</td>
<td>Reference design</td>
</tr>
<tr>
<td>H4</td>
<td>Breadth increased by 1.0m</td>
</tr>
</tbody>
</table>
| I3      | Breadth increased by 1.0m  
      | Freeboard increased by 0.8m |
| J1      | Breadth increased by 0.6m  
      | Freeboard increased by 0.2m |
| K1      | change internal subdivision |
| K2      | change internal subdivision as K1  
      | part of bulkhead deck watertight |
| K3      | change internal subdivision as K1  
      | Freeboard increased by 0.4m |
| L1      | change internal subdivision as K1  
      | Breadth increased by 0.2m |
Large cruise vessel – Meyer Werft & Carnival

Cost Effectiveness
NPV vs A
allowable costs to meet NetCAF limit vs A

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<th>L1</th>
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<tbody>
<tr>
<td>required index R</td>
<td>0.8597</td>
<td>0.8597</td>
<td>0.8597</td>
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<td>0.8597</td>
<td>0.8597</td>
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</tr>
<tr>
<td>attained index A</td>
<td>0.8621</td>
<td>0.9087</td>
<td>0.9288</td>
<td>0.9004</td>
<td>0.8719</td>
<td>0.8777</td>
<td>0.8754</td>
<td>0.8774</td>
</tr>
<tr>
<td>Change in A</td>
<td>0.0000</td>
<td>0.0466</td>
<td>0.0667</td>
<td>0.0383</td>
<td>0.0098</td>
<td>0.0156</td>
<td>0.0133</td>
<td>0.0153</td>
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Ungraded
Small Cruise – Fincantieri & RCCL

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Small Cruise – Fincantieri & RCCL

- Global changes (beam, freeboard)
- Local changes (internal subdivision, watertight decks)

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</tr>
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<tbody>
<tr>
<td>00</td>
<td>Reference design</td>
</tr>
<tr>
<td>01</td>
<td>Sill increased on external weathertight aft doors</td>
</tr>
<tr>
<td>02</td>
<td>Vs.01 + Deck 3 made watertight for comp n.2 and n.3</td>
</tr>
<tr>
<td>03</td>
<td>Vs.02 + Cross flooding section within DB void spaces improved adding pipes</td>
</tr>
<tr>
<td>04</td>
<td>Vs.03 + Two weathertight door added and a watertight door added on BK deck</td>
</tr>
<tr>
<td>05</td>
<td>Vs.04 + Increased Beam by 0.2m (new B=20.2m)</td>
</tr>
<tr>
<td>06</td>
<td>Vs.04 + Increased Beam by 0.5m (new B=20.5m)</td>
</tr>
<tr>
<td>07</td>
<td>Vs.06 + Increased freeboard by 0.25m</td>
</tr>
<tr>
<td>08</td>
<td>Vs.07 + Increased Beam by 0.5m (new B=21m)</td>
</tr>
<tr>
<td>09</td>
<td>Vs.04 + Increased Beam by 0.1m (new B=20.1m)</td>
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</table>
**Small Cruise – Fincantieri & RCCL**

### Version Description

<table>
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<tbody>
<tr>
<td>00</td>
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<tr>
<td>01</td>
<td>Sill increased on external weathertight aft doors</td>
</tr>
<tr>
<td>02</td>
<td>Vs.01 + Deck 3 made weathertight for comp n.2 and n.3</td>
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<tr>
<td>03</td>
<td>Vs.02 + Cross flooding section within DB void spaces improved adding pipes</td>
</tr>
<tr>
<td>04</td>
<td>Vs.03 + Two weathertight door added and a watertight door added on BK deck</td>
</tr>
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<td>Vs.04 + Increased Beam by 0.2m (new B=20.2m)</td>
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<td>Vs.04 + Increased Beam by 0.1m (new B=20.1m)</td>
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### Required index R

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### Attained index A

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### Change in A

<table>
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# Baltic RoPax – Meyer Turku & Color Line

<table>
<thead>
<tr>
<th>Length bp (m)</th>
<th>B (m)</th>
<th>T (m)</th>
<th>GT</th>
<th>Number of persons</th>
</tr>
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<tbody>
<tr>
<td>Ungraded</td>
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<td></td>
</tr>
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</table>
### Baltic RoPax – Meyer Turku & Color Line

- Global changes (beam, new hullform, subdivided double hull on bulkhead deck)
- Effect of LLH

<table>
<thead>
<tr>
<th>Phase</th>
<th>Version</th>
<th>Description</th>
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<tbody>
<tr>
<td>A</td>
<td>Reference design</td>
<td></td>
</tr>
<tr>
<td><strong>Phase 1</strong></td>
<td><strong>B (Option 1)</strong></td>
<td>Breadth increased by 40 cm</td>
</tr>
</tbody>
</table>
| **Phase 1** | **C (Option 2)** | Breadth increased by 20 cm  
Freeboard increased by 20 cm |
| **Phase 1** | **D (Option 3)** | Breadth increased by 40 cm  
Freeboard increased by 20 cm |
| **Phase 1** | **E (Option 4)** | Breadth increased by 40 cm  
Freeboard increased by 40 cm |
| **Phase 2** | **F (Option 5)** | As version D (opt. 3)  
subdivided double hull on bulkhead deck |
| **Phase 3** | **I (Option 6)** | As version F (opt. 5)  
impact of LLH |
| **Phase 3** | **J (Option 7)** | As version F (opt. 5)  
Subdivided Car Deck |
| **Phase 3** | **K2 (Option 8)** | As version F (opt. 5)  
No Lower Hold |
| **Phase 4** | **L (Option 9)** | As version F (opt. 5) + 40 cm more breadth  
Breadth increased by 80 cm  
Freeboard increased by 20 cm  
subdivided double hull on bulkhead deck |

Ungraded
## Baltic RoPax – Meyer Turku & Color Line

**Cost Effectiveness**

### NetCAF Limit vs A

<table>
<thead>
<tr>
<th>Phase</th>
<th>Version</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>Phase 1</td>
<td>A</td>
<td>Reference design</td>
</tr>
<tr>
<td>Phase 1</td>
<td>B (Option 1)</td>
<td>Breadth increased by 40 cm</td>
</tr>
<tr>
<td>Phase 1</td>
<td>C (Option 2)</td>
<td>Breadth increased by 20 cm, Freeboard increased by 20 cm</td>
</tr>
<tr>
<td>Phase 1</td>
<td>D (Option 3)</td>
<td>Breadth increased by 40 cm, Freeboard increased by 20 cm</td>
</tr>
<tr>
<td>Phase 1</td>
<td>E (Option 4)</td>
<td>Breadth increased by 40 cm, Freeboard increased by 40 cm</td>
</tr>
<tr>
<td>Phase 2</td>
<td>F (Option 5)</td>
<td>As version D (opt. 3) subdivided double hull on bulkhead deck</td>
</tr>
<tr>
<td>Phase 3</td>
<td>I (Option 6)</td>
<td>As version F (opt. 5) impact of LLH</td>
</tr>
<tr>
<td>Phase 3</td>
<td>J (Option 8)</td>
<td>As version F (opt. 5) Subdivided Car Deck</td>
</tr>
<tr>
<td>Phase 3</td>
<td>K2 (Option 8)</td>
<td>As version F (opt. 5) No Lower Hold</td>
</tr>
<tr>
<td>Phase 4</td>
<td>L (Option 9)</td>
<td>As version F (opt. 5) + 40 cm more breadth = Breadth increased by 80 cm Freeboard increased by 20 cm subdivided double hull on bulkhead deck</td>
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</tbody>
</table>

<table>
<thead>
<tr>
<th>Version</th>
<th>A</th>
<th>B opt 1</th>
<th>C opt 2</th>
<th>D opt 3</th>
<th>E opt 4</th>
<th>F opt 5</th>
<th>I opt 6</th>
<th>J opt 7</th>
<th>K2 opt 8</th>
<th>L opt 9</th>
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<tbody>
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<td>0.0344</td>
<td>0.0498</td>
<td>0.0460</td>
<td>0.0671</td>
<td>0.0168</td>
<td>0.0858</td>
<td>0.0716</td>
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</table>

Change in A

<table>
<thead>
<tr>
<th>Version</th>
<th>A</th>
<th>B opt 1</th>
<th>C opt 2</th>
<th>D opt 3</th>
<th>E opt 4</th>
<th>F opt 5</th>
<th>I opt 6</th>
<th>J opt 7</th>
<th>K2 opt 8</th>
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<tr>
<td>0.0000</td>
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<td>0.0460</td>
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<td>0.0858</td>
<td>0.0716</td>
<td>0.0826</td>
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Ungraded
Mediterranean Ropax – STX-France & Stena Line/Color Line

<table>
<thead>
<tr>
<th>Length bp (m)</th>
<th>B (m)</th>
<th>T (m)</th>
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<th>Number of persons</th>
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<tr>
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</table>
Mediterranean Ropax – STX-France & Stena Line/Color Line

- Internal subdivision
- Subdivided car deck
- Effect of LLH

<table>
<thead>
<tr>
<th>Version</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>Initial design</td>
<td></td>
</tr>
<tr>
<td>V0</td>
<td>New S Ropax (SLF55 formulation)</td>
</tr>
<tr>
<td>V1</td>
<td>Depth + 10cm</td>
</tr>
<tr>
<td>V12</td>
<td>Additional WT bulkheads below bulkhead deck</td>
</tr>
<tr>
<td>V21</td>
<td>Additional WT subdivisions above bulkhead deck</td>
</tr>
<tr>
<td>V13</td>
<td>Side casing based on V12*</td>
</tr>
<tr>
<td>V14</td>
<td>Increase in breadth + 20cm based on V12</td>
</tr>
</tbody>
</table>

*studied but not found to contribute significantly to raise A
Mediterranean Ropax – STX-France & Stena Line/Color Line

<table>
<thead>
<tr>
<th>Version</th>
<th>Description</th>
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<tbody>
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<tr>
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<td>Side casing based on V12*</td>
</tr>
<tr>
<td>V14</td>
<td>Increase in breadth + 20cm based on V12</td>
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*studied but not found to contribute significantly to raise A

**Required index R**

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<tr>
<th>Version</th>
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<th>2nd design step</th>
<th>3rd design step</th>
<th>4th design step</th>
</tr>
</thead>
<tbody>
<tr>
<td>Description</td>
<td>V1 - depth +10</td>
<td>V12 - Add bkds below BHD</td>
<td>V21 - Add bkds on car deck</td>
<td>V14 - Breadth increased</td>
</tr>
<tr>
<td>Required index R</td>
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<td>0.7777</td>
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**Attained index A**

<table>
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<th>1 design step</th>
<th>2nd design step</th>
<th>3rd design step</th>
<th>4th design step</th>
</tr>
</thead>
<tbody>
<tr>
<td>Description</td>
<td>V1 - depth +10</td>
<td>V12 - Add bkds below BHD</td>
<td>V21 - Add bkds on car deck</td>
<td>V14 - Breadth increased</td>
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**Change in A**

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<th>3rd design step</th>
<th>4th design step</th>
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<tbody>
<tr>
<td>Description</td>
<td>V1 - depth +10</td>
<td>V12 - Add bkds below BHD</td>
<td>V21 - Add bkds on car deck</td>
<td>V14 - Breadth increased</td>
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Ungraded
Small RoPax – KEH & Stena Line

- Change of freeboard

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<tbody>
<tr>
<td>Initial</td>
<td>Design</td>
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<tr>
<td>RCO1</td>
<td>Raise main deck + 30 cm</td>
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</tbody>
</table>

<table>
<thead>
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<th>Version</th>
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Cost Effectiveness

NetCAF limit vs A
Double ender ferry – KEH & Stena Line

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<tr>
<th>Length bp (m)</th>
<th>B (m)</th>
<th>T (m)</th>
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Double ender ferry – KEH & Stena Line

- Change of freeboard

<table>
<thead>
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<th>Description</th>
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<tbody>
<tr>
<td>Initial design</td>
<td></td>
</tr>
<tr>
<td>RCO1</td>
<td>Raise main deck + 30 cm</td>
</tr>
<tr>
<td>RCO2</td>
<td>Increase Beam +40 cm</td>
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</table>

<table>
<thead>
<tr>
<th></th>
<th>Initial</th>
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<td>0.0189</td>
<td>0.037</td>
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</tbody>
</table>

Cost Effectiveness

Ungraded
Summary RCOs collision

- High attained index possible
- For RoPax higher cost-effective RCOs can be found
- Large difference between RoPax and cruise
Watertight doors
Methodology

- Impact of open WTD calculated based on simplified collision attained index
  - Single door open
  - Multiple doors open, randomly selected
- Some RCO investigated
  - Category doors changed
  - Doors removed and replaced by additional stair cases
- Removal of doors sometime not cost effective
- Large variation of results between sample ships
- Taking into account the normal operation of WTD (normally closed, closing time 1 min.) there is no significant effect on attained index
Watertight doors
Summary

- Relation between connected volume and loss of index offers a great opportunity to increase awareness on board
  - Impact on safety level visible
  - Easy method, no damage stability calculation needed
  - May be used on board existing ships
- Designs without the need to operate WTD are possible for large ships
  - More restrictions for smaller ships
  - Difficult for ropax, as the WTD are needed to access spaces along the ship
- SDC2 decision to remove type A doors resolves much of the design problem
GROUNDING
Methodology

- Direct approach used
  - Bottom and side groundings
  - 5 repetitions with 10000 breaches each
  - Good approximation of A
- Internal watertight integrity not fully considered
- Explicit RCOs investigated for large cruise and mediterranean ropax only
- For remaining sample ships only recalculation of reference version and one collision RCO.
Global changes (beam, freeboard)

Local changes (double hull, WT decks)

<table>
<thead>
<tr>
<th>Version</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>G2</td>
<td>Reference design</td>
</tr>
<tr>
<td>G3</td>
<td>as G2 with deck 3 made watertight as far as possible</td>
</tr>
<tr>
<td>K3</td>
<td>Selected optimized version for collision change internal subdivision as K1 Freeboard increased by 0.4m</td>
</tr>
<tr>
<td>K4</td>
<td>as K3 with deck 3 made watertight as far as possible</td>
</tr>
<tr>
<td>M1</td>
<td>double hull increased DB height lengthened by 1 web frame</td>
</tr>
<tr>
<td>M2</td>
<td>as M1 with deck 3 made watertight as far as possible</td>
</tr>
<tr>
<td>I3</td>
<td>Breadth increased by 1.0m Freeboard increased by 0.8m</td>
</tr>
</tbody>
</table>
All grounding RCOs are cost effective
- some RCO do not comply with SOLAS2009 anymore
GROUNDING
Mediterranean RoPax – STX-France & Stena Line/Color Line

- Internal subdivision + beam increased
- WT decks + crossflooding

<table>
<thead>
<tr>
<th>Version</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>V0</td>
<td>original design</td>
</tr>
<tr>
<td>V14</td>
<td>Optimized for collision: Internal subdivision + Breadth increased</td>
</tr>
<tr>
<td>V15</td>
<td>Cross flooding devices + watertightness of longitudinal bulkheads</td>
</tr>
<tr>
<td>V16</td>
<td>Additional watertight parts of decks</td>
</tr>
</tbody>
</table>
GROUNDING
Mediterranean RoPax – STX-France & Stena Line/Color Line

- Internal changes are cost effective
- Change of main parameters are not cost-effective

<table>
<thead>
<tr>
<th>Version</th>
<th>V00</th>
<th>V14</th>
<th>V15</th>
<th>V16</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>original design</td>
<td>Optimized for collision: Internal subdivision + Breadth increased</td>
<td>Cross flooding devices + watertightness of longitudinal bulkheads</td>
<td>Additional watertight parts of decks</td>
</tr>
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<td>Collision SOLAS2009 +SLF55</td>
<td>0.8398</td>
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<td>0.958</td>
<td>0.963</td>
<td>0.973</td>
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</tbody>
</table>
GROUNDING
Summary

- High index for grounding can be attained
- Direct approach is very time consuming but offers great potential to be used also for collision
- Methodology requires further validation and confirmation by IMO
- Some RCOs improve collision and grounding, other RCOs have adverse effects on collision or grounding
- Effect on detailed design and internal watertight integrity to be further analysed
Sample ships, RCOs and CBA

- Introduction and overview of the EMSA III studies (Odd Olufsen)
- Formal Safety Assessment, Risk Models for collision and grounding (Rainer Hamann)
- Methodologies for assessing risk from watertight doors and risk from grounding (Odd Olufsen)
- Sample ships; design and risk control options (Henning Luhmann)
- Summary of results, recommendations for decision making (Odd Olufsen)
Effects of taking grounding into account in the CBA

Attained Index A (collision) for Risk control Options meeting the CAF criteria with and without including the effect from grounding.
N is the number of persons onboard without consideration of type of LSA
Alternative when grounding is accounted for in the CBA

\[ R = 1 - \frac{C1 \times 6200}{4 \times N + 20000} \]

\[ C1 = 0.8 - \frac{0.25}{10000} \times (10000 - N) \]

\( N \) is the number of persons onboard without consideration of type of LSA
Conclusions

- The project does not provide any data for RoPax and passenger ships carrying less than 400 persons onboard.
- There is no data available for RoPax having more than 3280 persons onboard.
- The Cost-Effectiveness Analysis performed in the project, supports raising the level of R for collision.
- For cruise ships, a number of RCOs have been investigated on 2 sample ships. When the assessment is based on benefits from collision only, the RCOs found to be cost effective show only limited improvement. Grounding represents a significantly higher risk than collision based on the calculations carried out in the project. There is a clear trend that RCOs improving the attained index A for collision would also improve the attained index A for grounding. When grounding is included in the risk assessment the CAF values are generally reduced and additional RCOs become cost-effective.
- Suggested levels of R are shown in two different formulations. Both formulations show a significant increase of safety level for small and medium sized ships and a moderate increase for very large ships. However, accounting for the additional cost-effective RCOs deriving from consideration of grounding (as explained above), it is concluded that the formulation with the higher level of R is deemed more appropriate, following closely the FSA process and methodology. *

* Some members of the consortium have expressed their reservation wrt. use of grounding in the CBA before the methods and assumptions have been further tested and validated.
Discussion points

- These include recommendations by the Project Partners as a Group of Experts and as Stakeholders of the maritime/marine industry beyond the EMSA III framework.
  - For large cruise ships, there is limited amount of information/data concerning their survivability in damaged conditions due to relatively small fleet and (luckily) small number of casualties, thus not attracting research focus. The limited amount that does exist indicates that the current formulation of the s-factor in SOLAS 2009 tends to underestimate the survivability of cruise ships. This, in turn, influences ΔPLL and cost-effectiveness.
  - By contrast, there are significantly more published validation results available for damage stability of RoPax ships (s-factor) than for cruise ships, e.g., North-West European Project for Damage Stability of Ro-Ro Passenger Ships (the basis for Stockholm Agreement) and the EC-funded projects HARDER and GOALDS.
  - The results of EMSA III show that grounding is the dominant risk. It certainly represents a significantly higher risk than collision. However, further validation and testing is required in order to develop specific proposals.
  - Presentation to and familiarisation by industry outside the consortium is also recommended before suggesting requirements such as combined collision and grounding to IMO.
  - Method and software for calculation of A for collision should be developed based on the non-zonal approach as was done in the EMSA III project for grounding.
Thank you for your kind attention

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